

• Form Factors & Structure factors

This is list of available form factor and structure factors in Irena package. This is current as of release of 2.55.

Content:

Form & Structure factors parameters

Form Factor description

Spheroid

Integrated_Spheroid

Cylinder

CylinderAR

removed in v2.62: Algebraic_Globules

removed in v2.62: Algebraic_Rods

removed in v2.62: Algebraic_Disks

Unified_Sphere

Unified_Rod

Unified_RodAR

Unified_Disk

CoreShell

CoreShellCylinder

CoreShellPrecipitate

Fractal Aggregate

CoreShellShell

SphereWHSLocMonoSq

Janus CoreShell Micelle 1

Janus CoreShell Micelle 2

Janus CoreShell Micelle 3

RectParallelepiped

User

Testing and using Form factors in users own code

Structure factors description

Interferences

HardSpheres

SquareWell

StickyHardSpheres

HayerPenfoldMSA

Interprecipitate

Calling the library and use

Form & Structure factors parameters

<u>Form Factor</u>	<u>Parameter(s)</u>
spheroid	AspectRatio = ParticlePar1
Integrated_Spheroid	AspectRatio=ParticlePar1
Cylinders	Length=ParticlePar1
CylindersAR	AspectRatio=ParticlePar1

Unified_Disc thickness = ParticlePar1
 Unified_Rod length = ParticlePar1
 Unified_RodAR AspectRatio = ParticlePar1
 Unified_Sphere none needed
 User uses user provided functions.
 There are two user provided functions necessary -
 F(q,R,par1,par2,par3,par4,par5)
 and V(R,par1,par2,par3,par4,par5)
 the names for these need to be provided in strings...
 the input is q and R in angstroms

Tube length=ParticlePar1 //length in A
 WallThickness=ParticlePar2 //in A
 CoreRho =ParticlePar3
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of core material
 ShellRho =ParticlePar4
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of shell material
 SolventRho =ParticlePar5
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of surrounding
 medium (air=0)

CoreShell CoreShellThickness=ParticlePar1 //skin thickness in Angstroms
 CoreRho =ParticlePar2
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of core material
 ShellRho =ParticlePar3
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of shell material
 SolventRho =ParticlePar4
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of surrounding
 medium (air=0)

CoreShellPrecipitate CoreShellThickness is calculated for each size, so the average contrast of
 the core+shell is same as contrast of the solvent.
 CoreRho =ParticlePar2
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of core material
 ShellRho =ParticlePar3
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of shell material
 SolventRho =ParticlePar4
 //rho [10¹⁰ cm-2] (not delta rho squared!!!) of surrounding
 medium (air=0)

Fractal aggregate FractalRadiusOfPriPart=ParticlePar1 //radius of primary particle
 FractalDimension=ParticlePar2 //Fractal dimension

SphereWHSLocMonoSq Distance for HS model as ratio to part radius
 Hard Spheres model fraction

Janus CoreShell Micelle 1 //particle size is total size of the particle
 (R0 in the figure in description)
 Shell_Thickness=ParticlePar1//shell thickness
 SolventRho=ParticlePar2 // rho for solvent
 CoreRho=ParticlePar3 // rho for core material
 Shell1Rho=ParticlePar4 // rho for shell 1
 Shell2Rho=particlePar5 // rho for shell 2

Janus CoreShell Micelle 2 //particle size here is shell thickness!!!
 Core_Size=ParticlePar1 // Core radius A
 SolventRho=ParticlePar2 // rho for solvent
 CoreRho=ParticlePar3 // rho for core material
 Shell1Rho=ParticlePar4 // rho for shell 1
 Shell2Rho=particlePar5 // rho for shell 2

Janus CoreShell Micelle 3 //particle size here is core radius

Shell_Thickness=ParticlePar1 // Shell Thickness A
 SolventRho=ParticlePar2 // rho for solvent
 CoreRho=ParticlePar3 // rho for core material
 Shell1Rho=ParticlePar4 // rho for shell 1
 Shell2Rho=ParticlePar5 // rho for shell 2
 RectParallelepiped //particle size here is side a
 Side B ratio =ParticlePar1 // Ratio side B/A
 Side C ratio=ParticlePar2 // Ratio side C/A

Structure factors included

Interferences reference: Beaucage, G. (1995). J Appl Crystallogr **28**, 717-728.

Par1: ETA (center-to-center distance)

Par2: Pack (number of particles In nearest neighbor sphere)

Hard Spheres reference: Percus-Yevick model, PERCUS,YEVICK PHYS. REV. 110 1 (1958), THIELE J. CHEM PHYS. 39 474 (1968), WERTHEIM PHYS. REV. LETT. 47 1462 (1981)

Par1: Radius [A]

Par2: Volume fraction (fraction)

Square Well reference: SHARMA,SHARMA, PHYSICA 89A,(1977),212, NOTE - depths >1.5kT and volume fractions > 0.08 give UNPHYSICAL RESULTS when compared to Monte Carlo simulations

Par1: Radius [A]

Par2: Volume fraction [fraction]

Par3: Well depth e/kT, dimensionless, positive values are attractive

Par4: Well width, multiples of diameters

Sticky hard spheres no reference given in NIST macrosÅc

Par1: Radius [A]

Par2: Vol. fraction

Par3: Perturbation parameter (0.1)

Par4: Stickiness, tau

Hayer Penfold MSA no reference given in NIST macrosÅc

Par1: Radius [A]

Par2: Charges

Par3: Volume fraction

Par4: Temperature in Kelvin

Par5: Monovalent salt concentration (M)

Par6: dielectric constant of solvent

Interprecipitate SF Formula 6 in APPLIED PHYSICS LETTERS 93, 161904 (2008)Åc

Par1: Distance L [A]

Par2: Sigma (root-mean-square deviation (ordering factor))

Important comment for Core-shell and Core shell cylinder (and Unified tube)

The volume definition for Core-shell objects is matter of discussion. Heated at times and I suspect that the appropriate answer depends on the case when and how the FF is used. Therefore from version 2.26 Irena macros include option which needs to be set - both Core shell and Core shell cylinder will share common parameter (this parameter is global for all cases of calls to core shell form factors or their volumes) of volume definition.

The options are: whole particle, core, and shell.

Note: Unified tube is using as volume the volume of shell. It is how it is defined at this time and it is meant for cases like Carbon nanotubes, when this is appropriate. To match with core shell cylinder us "shell" as volume

Use of optional xop from NIST package

Since 2.53 version, some of the form factors are ONLY available if NIST form factor xop is installed on the computer (*Parallelepiped*) or can take advantage of the speed improvements, when the xop is installed (*Cylinders*, *Spheroid*). If you install NIST SANS package:

http://www.ncnr.nist.gov/programs/sans/data/red_anal.html

it installs xop which provides fast calculations of the various form factors.

If you use these form factors, cite (*in addition to Irena manuscript*) also Steven Kline manuscript for NIST package: "Reduction and Analysis of SANS and USANS Data using Igor Pro", Kline, S. R. J Appl. Cryst. 39(6), 895 (2006).

Form Factor description

Spheroid

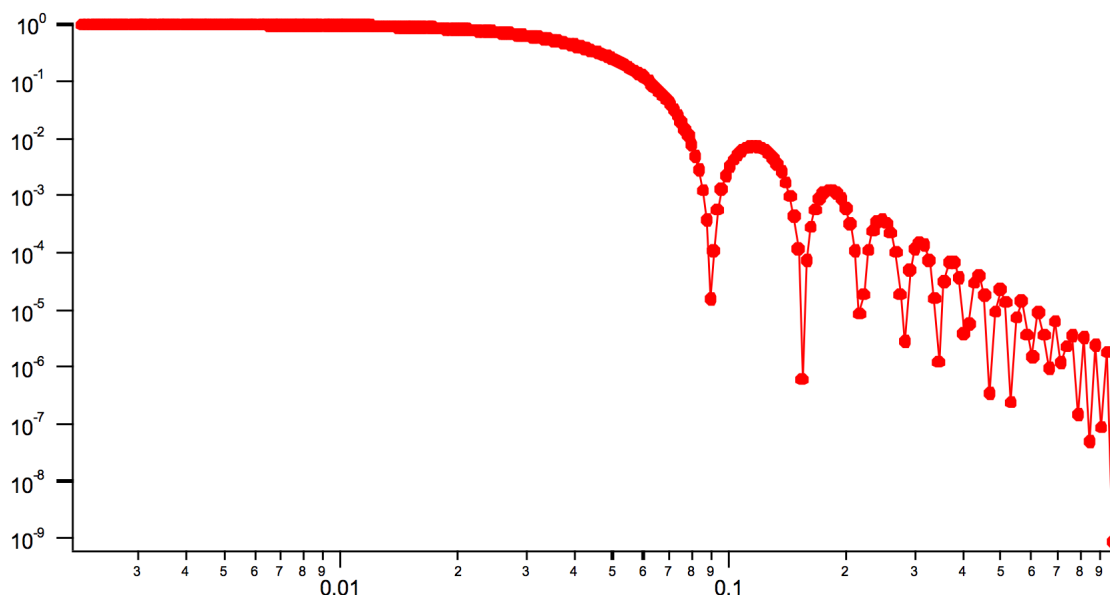
uses sphere form factor for aspect ratio between 0.99 and 1.01:

$$F^2 = 3/(QR^3)) * (\sin(QR) - (QR * \cos(QR)))$$

$$\text{volume : } V = ((4/3) * \pi * \text{radius}^3)$$

This calculation approximates integral over R as rectangle (compare with Integrated spheroid).

graph for R = 50A



For aspect ratios smaller than 0.99 and larger than 1.01 uses standard form factor for

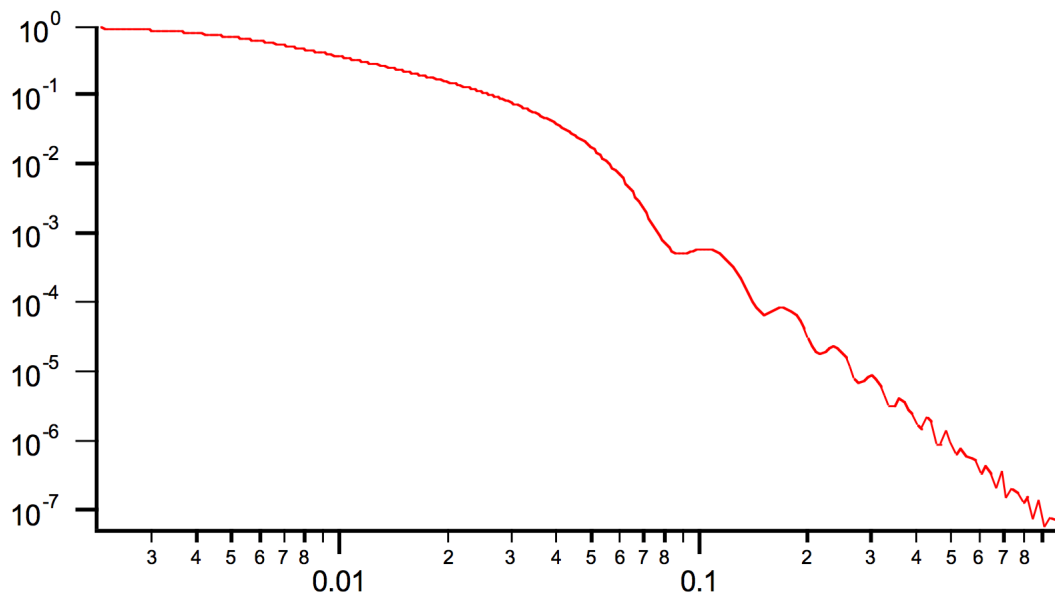
spheroid:

$$F = \text{Integral of } (3/(QR^3)) * (\sin(QR) - (QR * \cos(QR)))$$

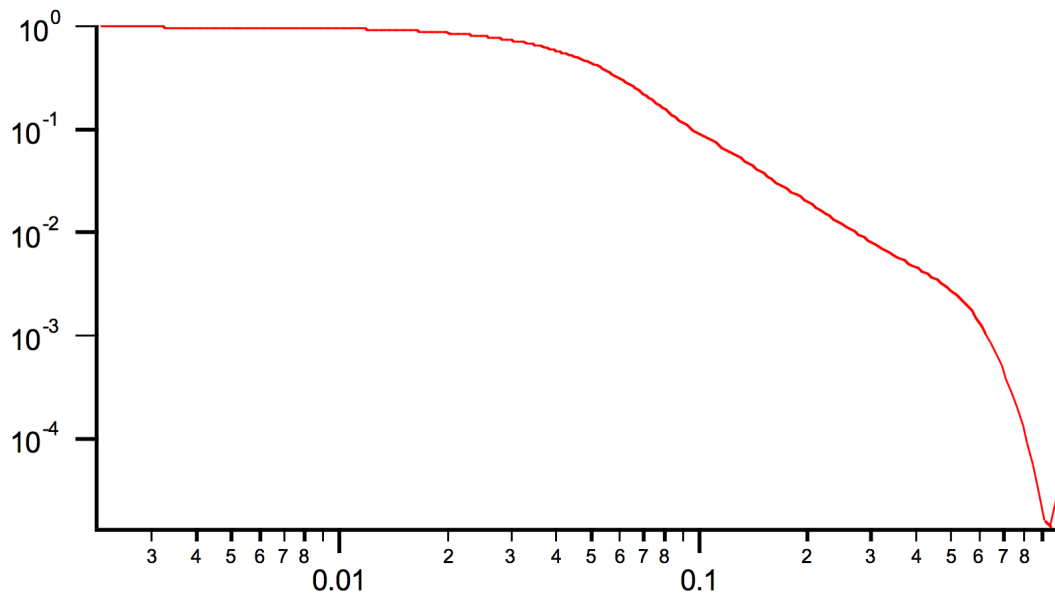
$$\text{where } QR = Q_{\text{value}} * \text{radius} * \sqrt{1 + (((AR^2) - 1) * \cos^2 \theta)}$$

over of $\cos \theta = 0$ to 1. This is numerically calculated using 50 points (step in $\cos \theta = 0.02$). Following graphs are examples:

AR = 10



AR=0.1



Since Irena version 2.54 Spheroid with aspect ratio !=1 will use NIST xop to speed up its calculations, if this xop is available. See note above.

Integrated_Spheroid

same code as in the spheroid, but in this case the code integrates over the width of the R bin.

Note, the bin start and end points are calculated linearly (even for log-binned data) as half way distance:

$$R_{\text{start}} = (R_n + R_{n-1})/2$$

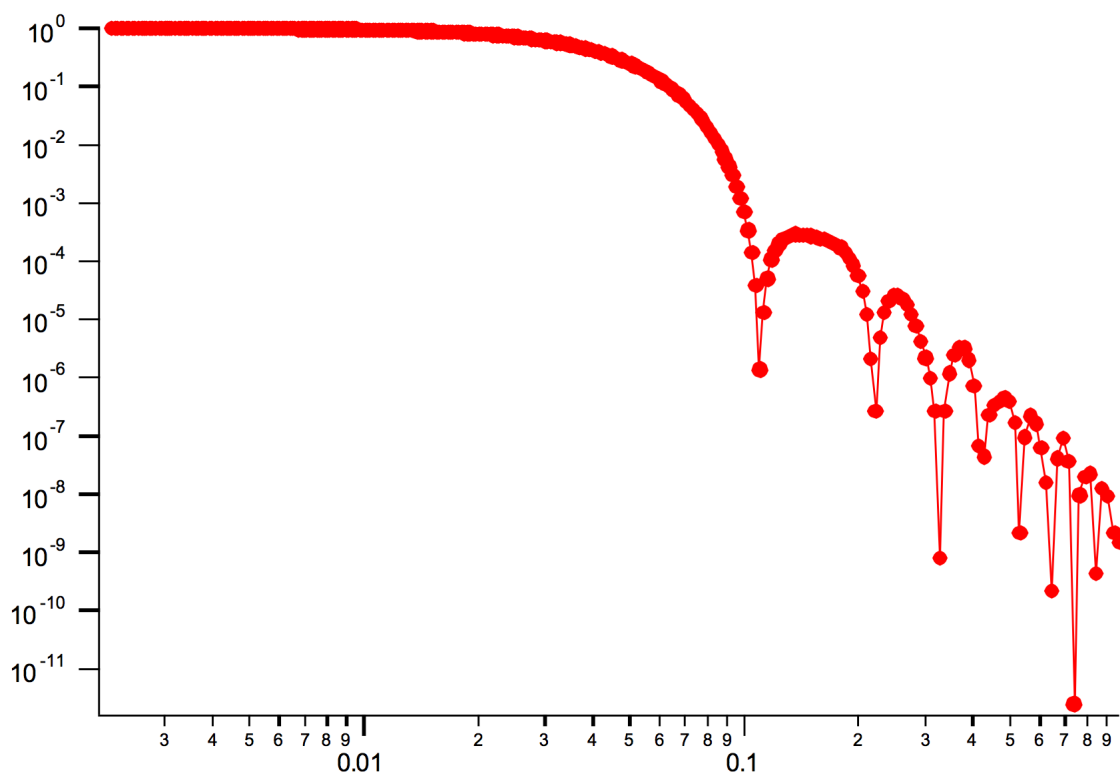
$$R_{\text{end}} = (R_n + R_{n+1})/2$$

Uses adaptive steps to integrate essel function oscillations of the form factor over the width of the bin in R - note, the averaging is done including the volume of particles involved. This code is quite convoluted and time consuming. Its only reasonable use is for cases with wide bins in radius (R), when this removes some of the bessel function oscillations.

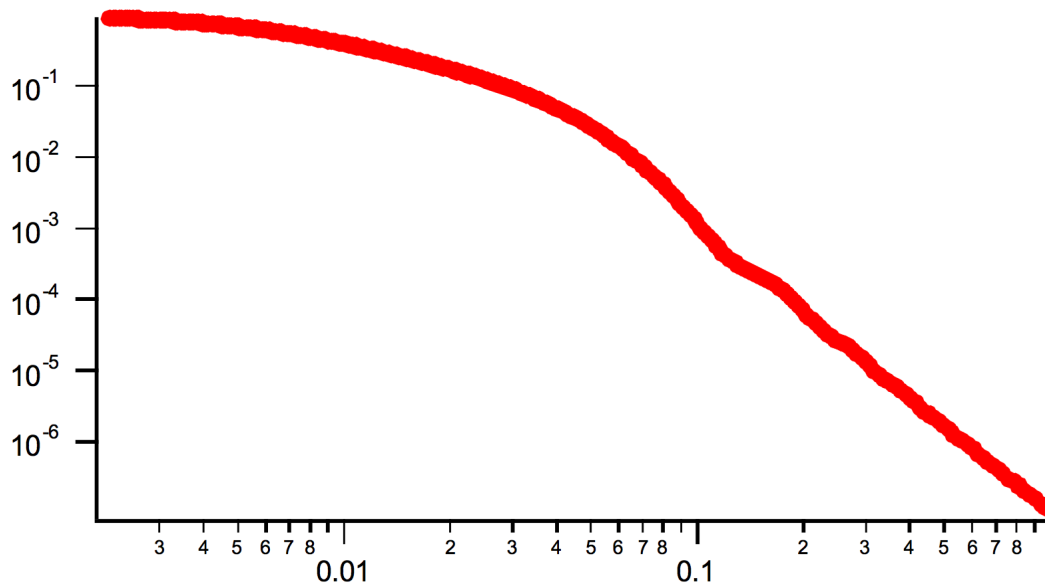
Examples with R width 40A, average size 50A (that means R varies from 30 to 70A).

Note that the bessel function oscillations are somewhat smooth out. With wider bins in R these oscillations may disappear all together.

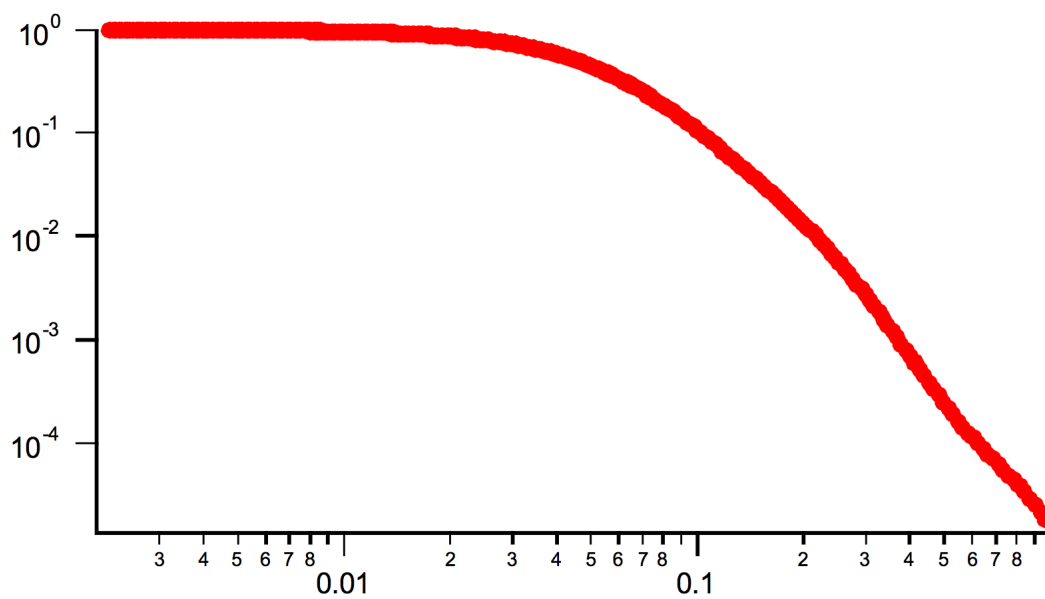
AR = 1 (sphere)



AR=10 (Spheroid)



AR=0.1 (spheroid)



Cylinder

CylinderAR

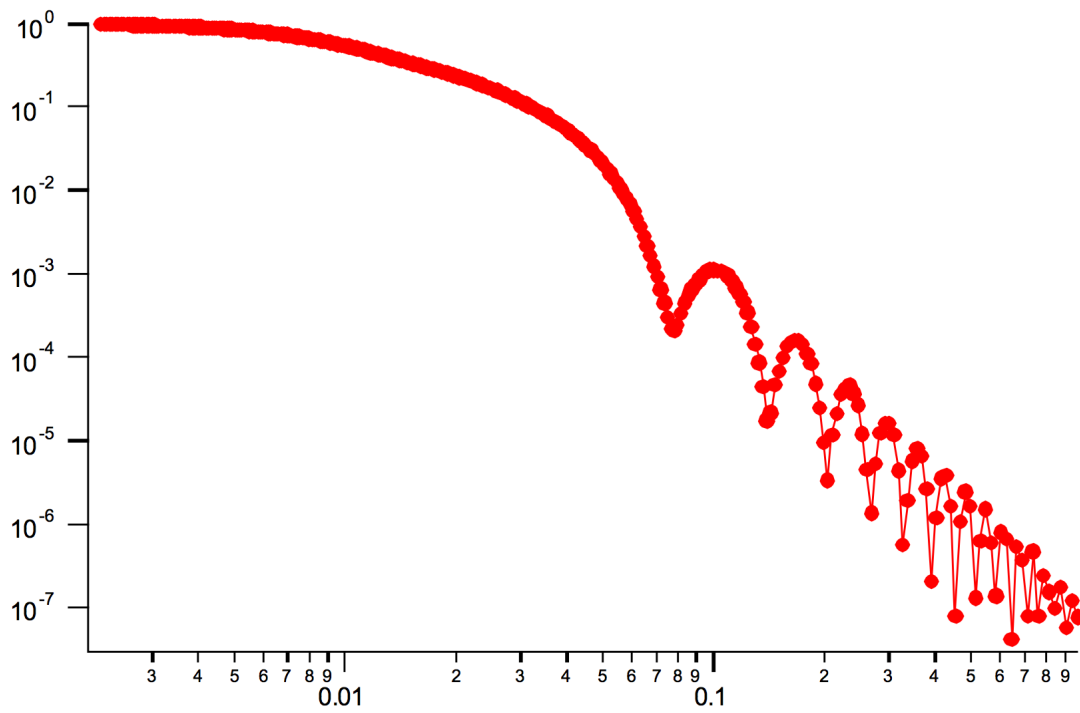
The code uses the following code to calculate form factor for cylinder. Note, that also this code is doing the same integration as integrated spheroid above (see 2).

Form factor = integral over (Ft) for Alpha = 0 to $\pi/2$, Ft is below:
 $\text{LargeBes} = \sin(0.5 * Q\text{value} * \text{length} * \cos(\text{Alpha})) / \text{LargeBesArg}$

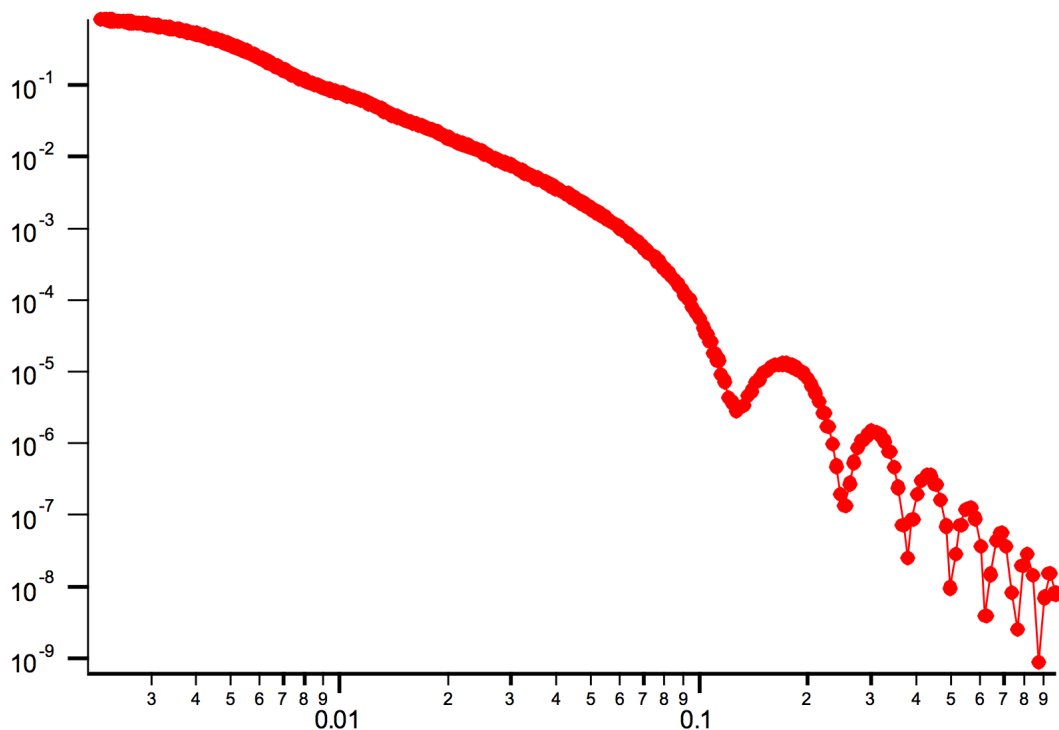
```
SmallBessDivided=BessJ(1, Qvalue*radius*Sin(Alpha))/Qvalue*radius*Sin(Alpha)  
Ft = LargeBes*SmallBessDivided
```

Examples

Cylinder with length 500A and radius 50A.



Disk (cylinder) with radius 500A and length 50A.



Since Irena version 2.54 Cylinders will use NIST xop to speed up its calculations, if this xop is available. See note above.

removed in v2.52: **Algebraic_Globules**

removed in v2.52 - use Unified FF approximation (it is much better)

removed in v2.52: **Algebraic_Rods**

removed in v2.52 - use Unified FF approximation (it is much better)

removed in v2.52: **Algebraic_Disks**

removed in v2.52 - use Unified FF approximation (it is much better)

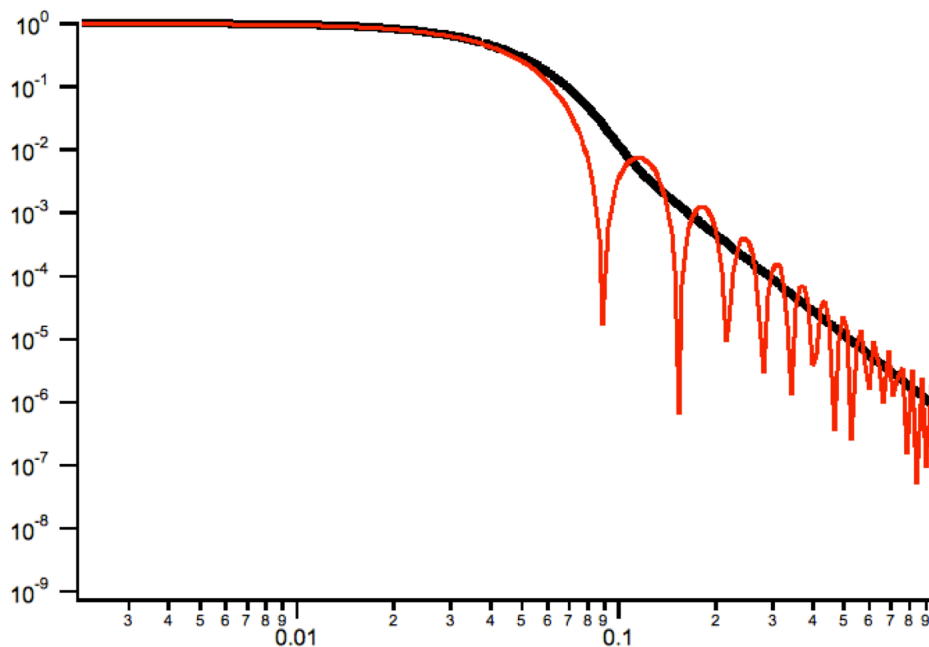
Unified_Sphere

This is formula from Unified fit model by Greg Beaucage (see Unified tool and documentation for it). The parameters are calculated from the code in the manual for each different shape. Specific formulas for these shapes were provided by Dale Schaefer...

This is the code:

```
G1=1
P1=4
Rg1=sqrt(3/5)*radius
B1=1.62*G1/Rg1^4
QstarVector=qvalue/(erf(qvalue*Rg1/sqrt(6)))^3
F^2 = G1*exp(-qvalue^2*Rg1^2/3)+(B1/QstarVector^P1)
```

Example for R=50A compared with the spheroid with aspect ratio =1



Unified_Rod

Unified_RodAR

This is formula from Unified fit model by Greg Beaucage (see Unified tool and documentation for it). The parameters are calculated from the code in the manual for each different shape. Specific formulas for these shapes were provided by Dale Schaefer...

This is the code:

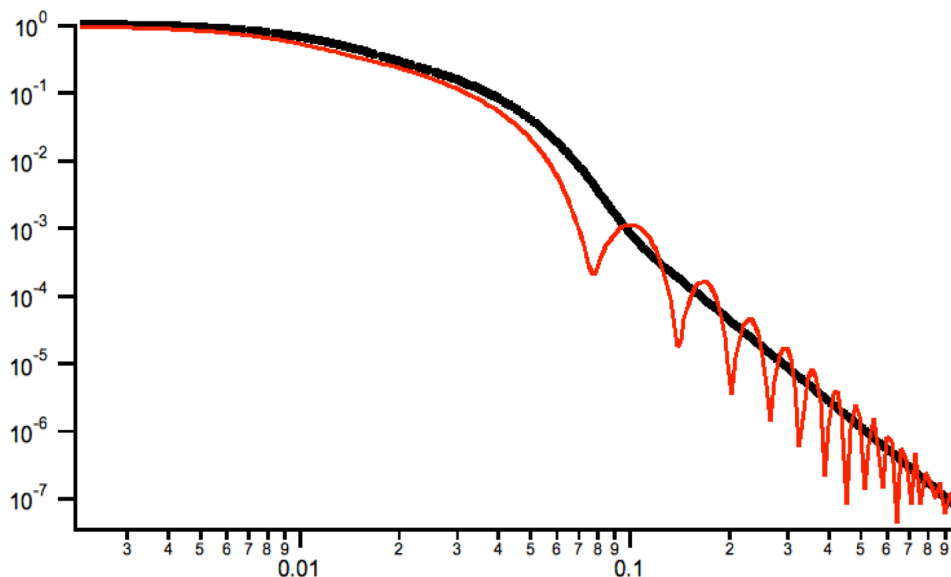
```
G2 =1
Rg2=sqrt(Radius^2/2+Length^2/12)
B2=G2*pi/length
P2=1
```

```

Rg1=sqrt(3)*Radius/2
RgC02=Rg1
G1=2*G2*Radius/(3*Length)
B1=4*G2*(Length+Radius)/(Radius^3*Length^2)
P1=4
QstarVector=qvalue/(erf(qvalue*Rg2/sqrt(6)))^3
A=G2*exp(-qvalue^2*Rg2^2/3)+(B2/QstarVector^P2) * exp(-RGC02^2 * qvalue^2/
QstarVector=qvalue/(erf(qvalue*Rg1/sqrt(6)))^3
F^2 = A + G1*exp(-qvalue^2*Rg1^2/3)+(B1/QstarVector^P1)

```

Example for R=50A and length 500A compared with the cylinder



```

*****
*****
*****
*****

```

Unified_Disk

This is formula from Unified fit model by Greg Beaucage (see Unified tool and documentation for it). The parameters are calculated from the code in the manual for each different shape. Specific formulas for these shapes were provided by Dale Schaefer...

This is the code:

```

G2=1
Rg2=sqrt(Radius^2/2+thickness^2/12)
B2=G2^2/(radius^2)//dws guess
P2=2
Rg1=sqrt(3)*thickness/2// Kratky and glatter = Thickness/2
RgC02=1.1*Rg1
G1=2*G2*thickness^2/(3*radius^2)
B1=4*G2*(thickness+Radius)/(Radius^3*thickness^2)//same as rod
P1=4

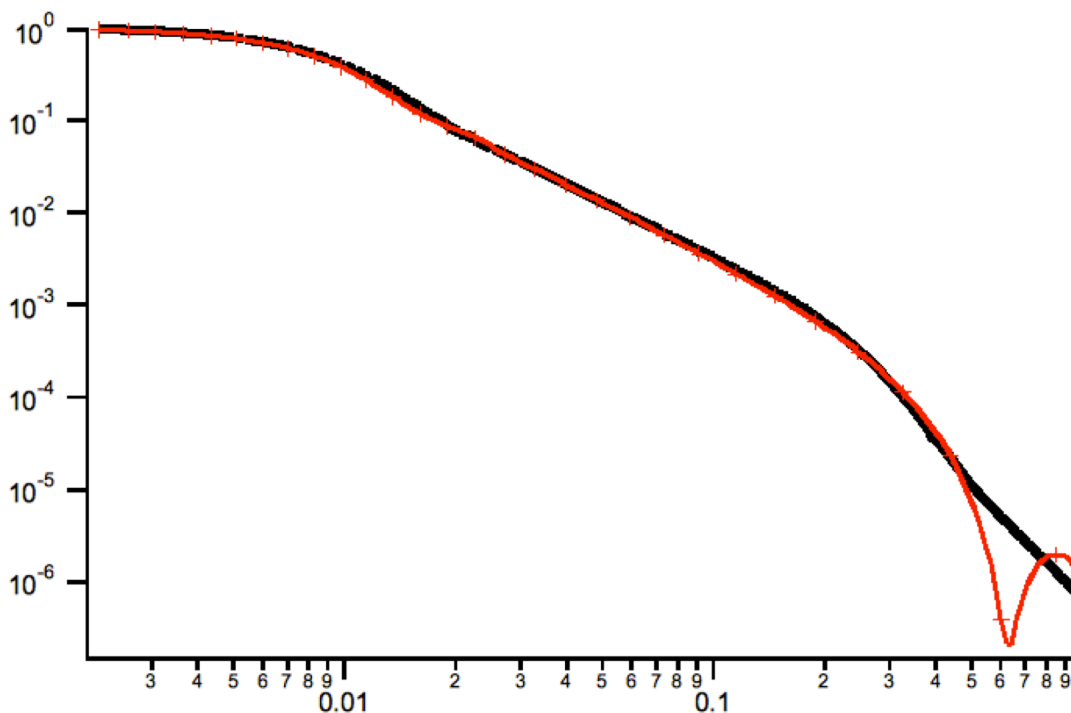
```

```

QstarVector=Q/(erf(Q*Rg2/sqrt(6)))^3
A=G2*exp(-Q^2*Rg2^2/3)+(B2/QstarVector^P2) * exp(-RGC02^2 * Q^2/3)
QstarVector=Q/(erf(Q*Rg1/sqrt(6)))^3
F^2 = A + G1*exp(-Q^2*Rg1^2/3)+(B1/QstarVector^P1)

```

Example for R=250Å and thickness 10Å compared with the cylinder



```

*****
*****
*****
*****

```

CoreShell

One thing to remember: the total radius of this particle is core radius + shell thickness...

If you use diameter as dimension of the particle (new in Irena version 2.53), the total diameter of the particle is diameter+2*shell thickness.

Note, this form factor calculation also includes integration over the width of bin in radii (same as integrated spheroid and cylinder).

Note: Input form factor parameter for core/shell/solvent is ρ in $[10^{10} \text{ cm}^{-2}]$ - this is very important to keep in mind.

Note, that there is volume definition choice you need to do: Whole particle, core, or shell, as appropriate for given problem. This volume definition is used for all volume calculations for this particle. It is global parameter for all core shell cylinder or core shell calls in the WHOLE EXPERIMENTAc.

Code (heavily simplified!):

```

RhoDelta = CoreRho - ShellRho
//core
Result1=(3/(Q*R)^3)*(sin(Q*R)-(Q*R*cos(Q*R))) * RhoDelta * (4/3 * pi * R^3)

//Now add the shell (skin) , thickness Rshell
r = R+Rshell
RhoDelta = ShellRho - SolventRho
Result2 = (3/(Q*r)^3)*(sin(Q*r)-(Q*r*cos(Q*r))) * RhoDelta * (4/3 * pi * r^3)

//summ them together and normalize by the total particle volume
F^2 =( result1 + result2 )^2 / Volume

```

Volume definition depends on the setting of above discussed global parameter and is either:

Whole particle volume = $\frac{4}{3} * \pi * (R+r)^3$

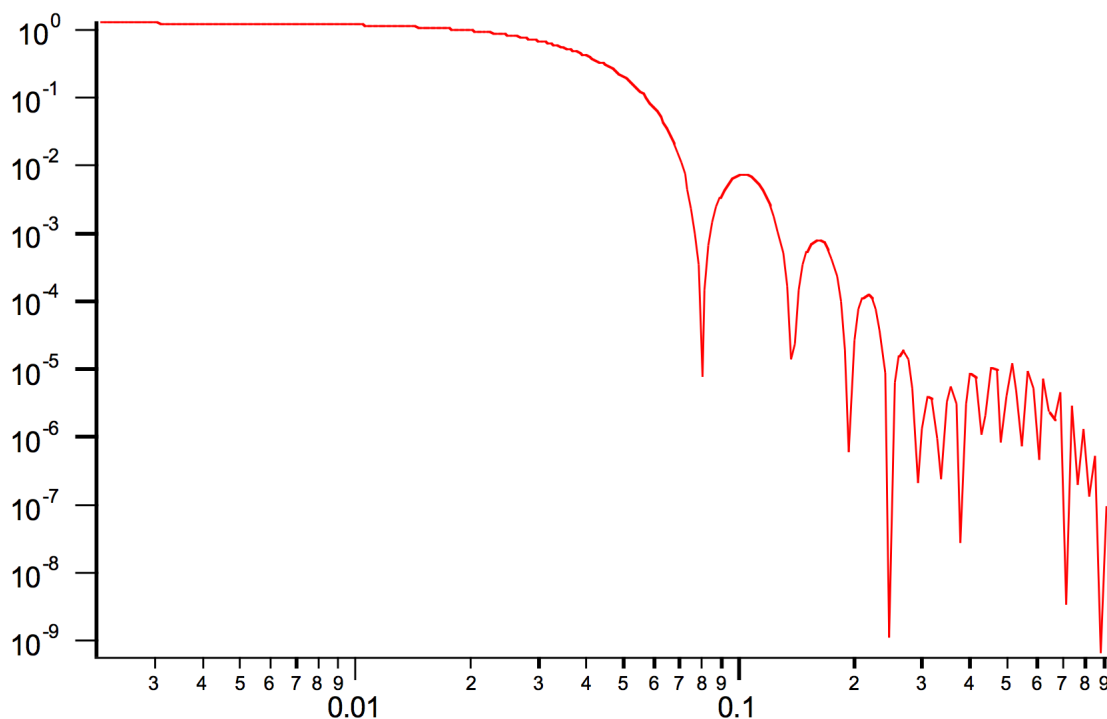
Core volume = $\frac{4}{3} * \pi * R^3$

Shell volume = $\frac{4}{3} * \pi * (R+r)^3 - \frac{4}{3} * \pi * R^3$

Make sure your choice is appropriate

Note, that to my surprise these calculations (copied from NIST Form factors) do not normalize correctly to 1 at low q . The reason is that the weighting is done by volume and contrast. I'll need to look into this again and in detail...

Example, Radius 50A, skin thickness 10A, contrast ratio 0.6



```

*****
*****
*****
*****

```

CoreShellPrecipitate

This is unique form factor, which - even for dilute sytem - results in "diffraction peak" type scattering. It is a very special case, when coreshell particle is formed from matrix and as it is formed, the core chemistry/rho deviates from matrix chemistry/rho. If the diffusion in the matrix is not fast enough, the chemistry around the particle changes, which results in rho changing in the other direction. Therefore one can end with coreshell particle which has higher-then-solvent rho core surounded by lower-then-solvent rho shell (or the other way). With average rho same as matrix. In such case at low-qs the particle "disappers" since we are probing material on larger length scales, and on average at those length scales the rho is the same. Fro example of this type of precipitation see:

Imhoff, S.D., et al., Kinetic transition in the growth of Al nanocrystals in Al-Sm alloys. *Journal of Applied Physics*, 2012. 111(6): p. 063525-9.

Remember, that by basic nature of this logic, the rho of the core/shell needs to be one larger and the other smaller than solvent rho. Also, they probably need to be pretty close together. If this is not correct, the code would create negative shell thicknesses and abort. Do not do it, it is not very physical...

The particle volume is always volume of the core. I think no other logic makes too much sense.

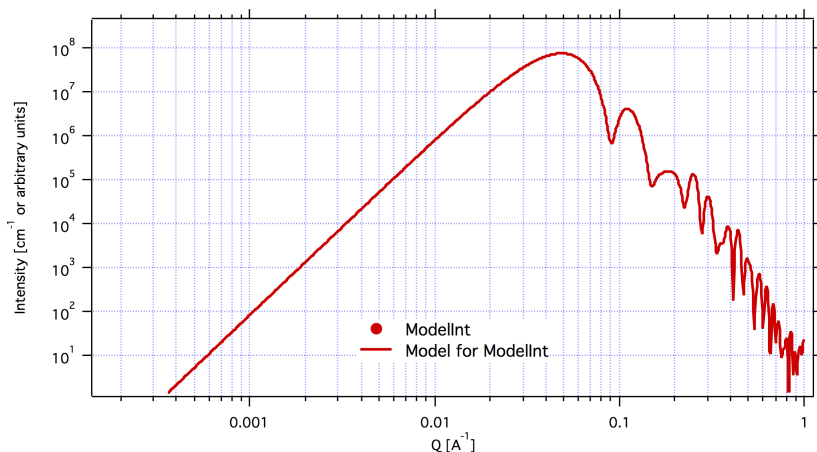
Code uses regular coreshell form factor (see above). For each size the shell thickness is calculated so the average rho of the particle matches the rho of the solvent. First we calculate:

$$\text{ShellVolume} = \text{CoreVolume} * (\text{SolventRho} - \text{CoreRho}) / (\text{ShellRho} - \text{SolventRho})$$

Then we calculate the shell thickness for known ShellVolume and known core radius.

$$\text{Core volume} = 4/3 * \pi * R^3$$

Example, Radius 50A, Core Rho 110, Shell Rho 85, Solvent Rho 90; note, this internally resolves to shell thickness of 35.5A.



```

*****
*****
*****
*****

```

CoreShellCylinder

Note, this form factor calculation also includes integration over the width of bin in radii (same as integrated spheroid and cylinder).

This code has been developed some time ago and I am not sure about it's function...

Code which is being used is direct copy of NIST Core shell cylinder.

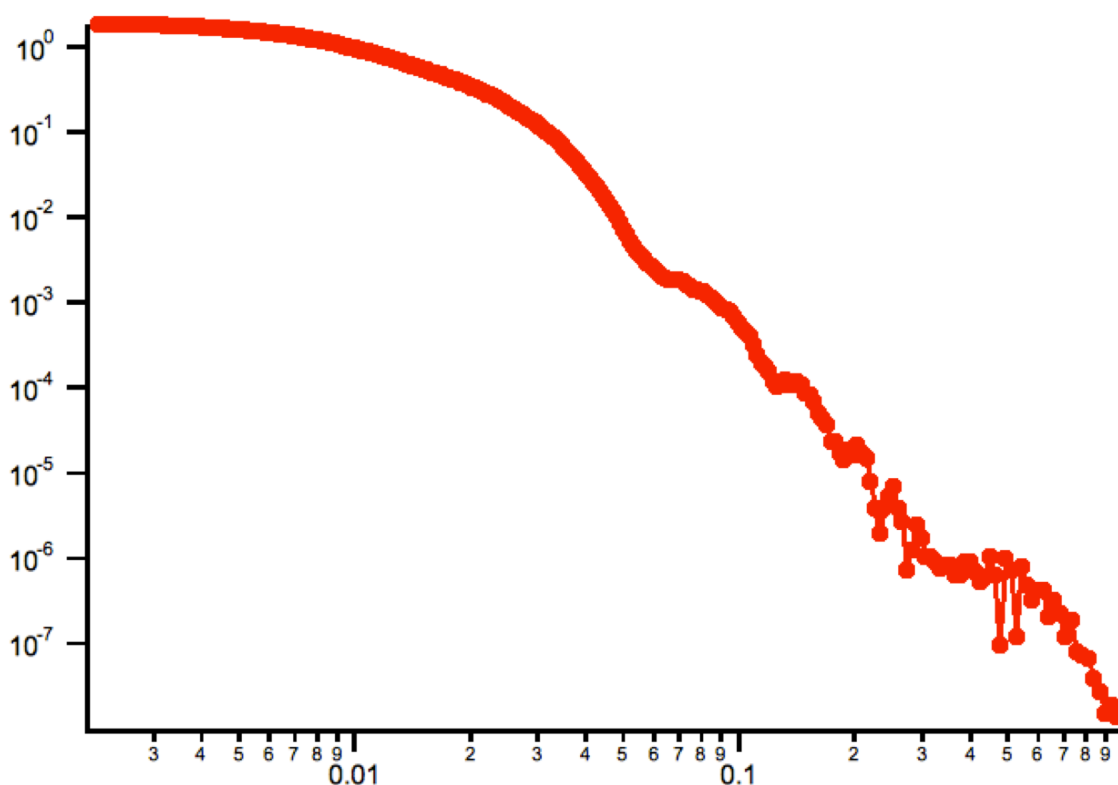
Note, that there is volume definition choice you need to do: Whole particle, core, or shell, as appropriate for given problem. This volume definition is used for all volume calculations for this particle. It is global parameter for all core shell cylinder or core shell calls in the WHOLE EXPERIMENTAc.

Volume definition depends on the setting of above discussed global parameter and is either:

Whole particle volume = $\pi * (R+r)^2 * (L+2*r)$

Core volume = $\pi * R^2 * L$

Shell volume = $\pi * (R+r)^2 * (L+2*r) - \pi * R^2 * L$



```

*****
*****
*****

```

Fractal Aggregate

This form factor was requested by Dale Schaefer and I cannot very well guarantee its functionality....

code:

```
f = IR1T_CalcSphereFormFactor(Qw[p],(2*Param1))
//calculates the F(Q,r) part fo formula
//this is same as for sphere of diameter = 2*Param1
//(= radius of primary particle, which is hard sphere)
//fractal part is next
F^2 = f^2 * IR1T_CalculateFractAggSQPoints(Qw[p],currentR,Param1, Param2)
```

where

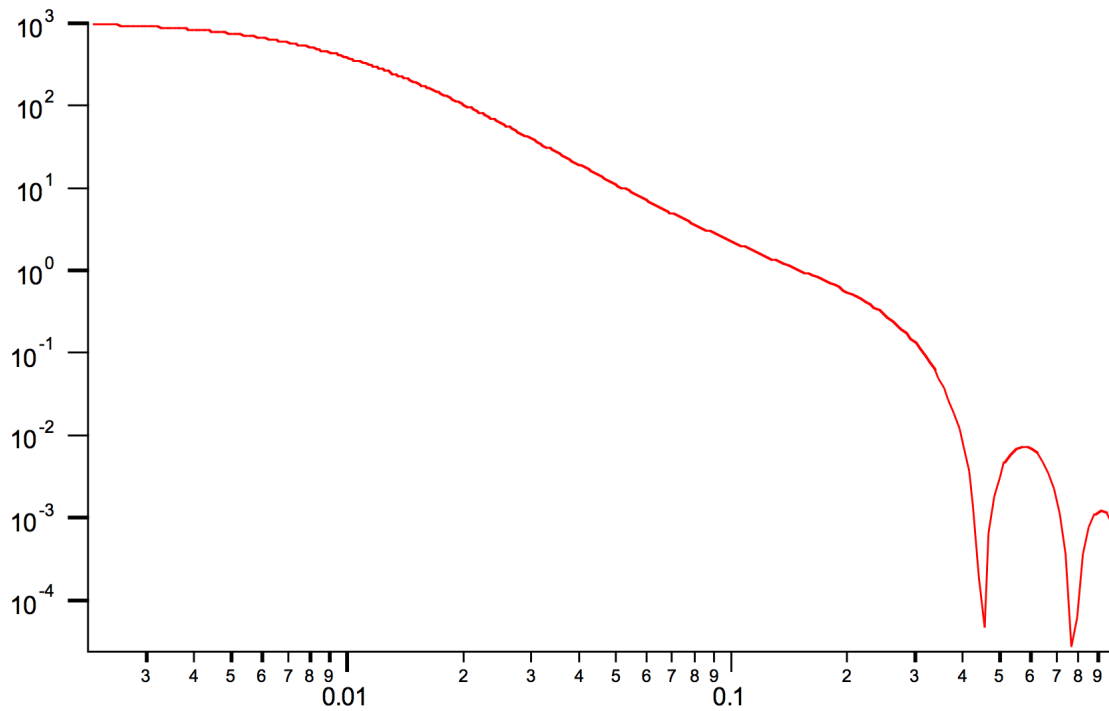
```
IR1T_CalculateFractAggSQPoints(Qvalue,R,r0, D) is
  QR=Qvalue*R
  part1=1
  part2=(qR*r0/R)^-D
  part3=D*(exp(gammln(D-1)))
  part5= (1+(qR)^-2)^((D-1)/2)
  part4=abs(sin((D-1)*atan(qR)))
  return (part1+part2*part3*part4/part5)
```

Note, that parameters are :

Param1 - radius of primary particle

param2 - fractal dimension of the fractal particles

Example for R=100A, radius of primary particle 10 A and fractal dimension 2.5.



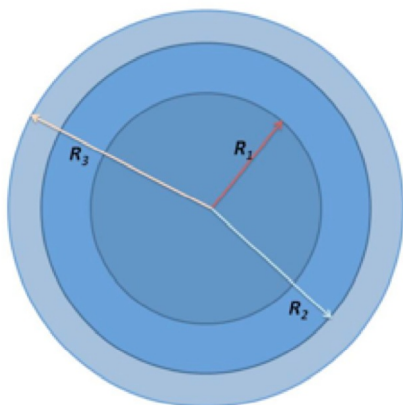
Comment: Note, that this is not scaled correctly at all... I have no idea why - apparently this formula is either wrongly coded or plainly does not behave right.

```
*****
*****
*****
*****
```

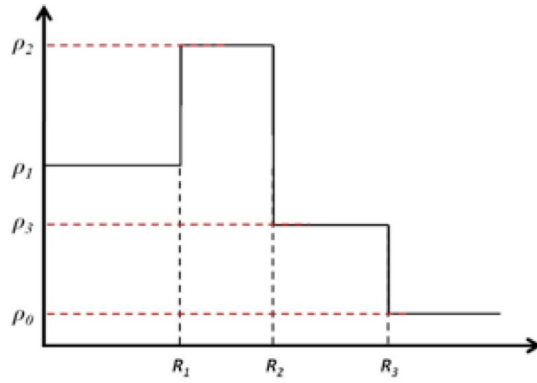
CoreShellShell

This form factor has been provided by Fan Zhang, many thanks to him.

Description of the model:



Scattering Length Density Rho:



List of Model Parameters:

R_1 : core radius

R_2 : outer radius of the first shell

R_3 : outer radius of the second shell

ρ_0 : scattering length density of the matrix

ρ_1 : scattering length density of the core

ρ_2 : scattering length density of the first shell

ρ_3 : scattering length density of the second shell

First-order Bessel function of the first kind is defined as

$$J_1(x) = \frac{\sin(x) - x \cos(x)}{x^2}$$

Volume is defined as

$$V_i = \frac{4\pi}{3} R_i^3$$

Form factor of the core-shell-shell structure is:

$$F(q) = \frac{3V_1}{qR_1}(\rho_1 - \rho_2)J_1(qR_1) + \frac{3V_2}{qR_2}(\rho_2 - \rho_3)J_1(qR_2) + \frac{3V_3}{qR_3}(\rho_3 - \rho_0)J_1(qR_3)$$

Volume definition depends on the setting of global parameter described in Core-shell form factor

and is either:

Whole particle volume = $\frac{4}{3} * \pi * (R+r)^3$

Core volume = $\frac{4}{3} * \pi * R^3$

Shell volume = $\frac{4}{3} * \pi * (R+r)^3 - \frac{4}{3} * \pi * R^3$

Where shell thickness "r" is sum of the two shell thicknesses ($R_3 - R_1$).

Make sure your choice is appropriate

```
*****
*****
*****
*****
```

SphereWHSLocMonoSq

This is form factor combined with structure factor – Based on Jan Skov Pedersen J. Appl. Cryst paper : J. Appl. Cryst. (1994) 27, 595-608. The model is locally mono dispersed system, therefore locally one can use spheres Form factor combined with structure factor.

For each bin here the code calculates $F(Q,R)^2 * S(Q,D,\phi)$, where $D \sim R$ via input parameter. Phi is simply fraction of Percus Yevic structure factor.

The result is different than multiplying dilute system by Structure factor – that assumes that the distance for Structure factor is the same for all sizes. In this case the ratio of distance to size of particle is the same. We assume here that the phi is the same for all sizes.

Suffise to say, that using this form factor with another structure factor is meaningless and garbage will be produced.

```
*****
*****
*****
```

Janus CoreShell Micelle 1

Janus CoreShell Micelle 2

Janus CoreShell Micelle 3

This is form factor based on manuscript:

T. Futterer, G. A. Vliegenthart, and P. R. Lang, "Particle Scattering Factor of janus Micelles", Macromolecules 2004, 37, 8407-8413.

The Form factor follows formula 3 of this manuscript

$$b_j^2(\mathbf{Q}, \theta) = \frac{4\pi^2}{Q^2(1-\mu^2)V_n^2} \left(((\rho_B + \rho_C) \int_0^{R_o} \cos(kz) F(R_o, z, \mu) dz \right. \\
+ (\Delta_{BA} + \Delta_{CA}) \int_0^{R_i} \cos(kz) F(R_i, z, \mu) dz)^2 \\
+ ((\rho_B - \rho_C) \int_0^{R_o} \sin(kz) F(R_o, z, \mu) dz \\
+ (\Delta_{BA} - \Delta_{CA}) \int_0^{R_i} \sin(kz) F(R_i, z, \mu) dz)^2 \Big)$$

where $Q=|\mathbf{Q}|$, $\mu=\cos\theta$, $k=Q\mu$, $\Delta_{BA}=\rho_A-\rho_B$, $\Delta_{CA}=\rho_A-\rho_C$ and the functions $F(R_j, z, \mu)$ are given by

$F(R_j, z, \mu) = \sqrt{R_j^2 - z^2} J_1(Q\sqrt{1-\mu^2}\sqrt{R_j^2 - z^2})$, with J_1 the Bessel function of first order. For this

structure the normalization constant is $V_n = \frac{2}{3} \pi ((\rho_B + \rho_C) \cdot (R_o^3 - R_i^3) + 2\rho_A \cdot R_i^3)$.

which describes scattering from the particle on the left of the Figure 1 from their manuscript (below).

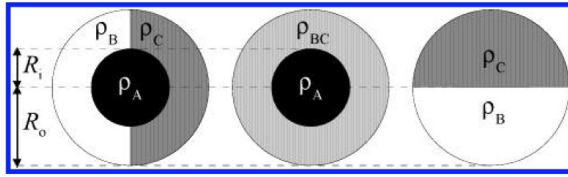
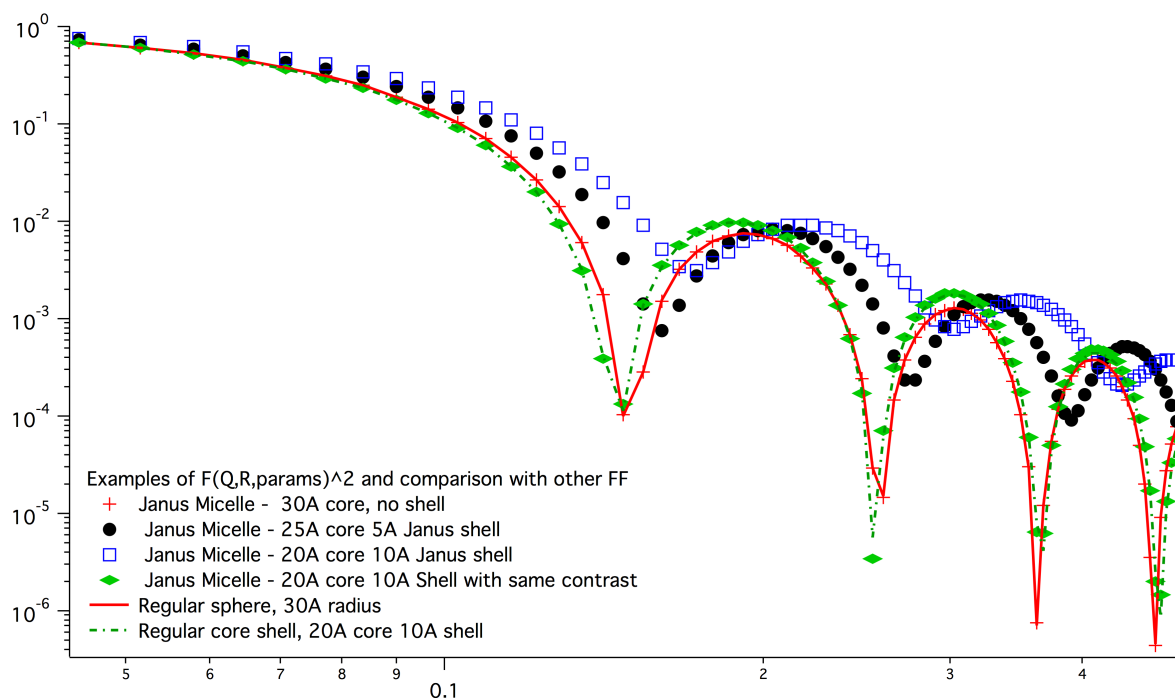


Figure 1. Sketch of competing particle structures. From left to right: Janus micelle, core-shell particle, and simplified Janus micelle.

Example of results:



Note: the results in the above graph are scaled to $F^2(Q=0) = 1$. Since the formula included scattering length densities, normalization by the volume does not result in $F^2(Q=0) = 1$. This may result in unexpected problems with absolute calibration.

This FF is implemented twice...

"Janus CoreShell Micelle 1" ... particle size is total size of the particle (R_0 in the figure in description), parameters:

```

Shell_Thickness=ParticlePar1           //shell thickness A
CoreRho=ParticlePar2                   // rho for core material
Shell1Rho=ParticlePar3                 // rho for shell 1 material
Shell2Rho=particlePar4                 // rho for shell 2 material
SolventRho=ParticlePar5                // rho for solvent material

```

"Janus CoreShell Micelle 2" ... particle size here is shell thickness!!! This may be very confusing!!!!, parameters:

```

Core_Size=ParticlePar1                 // Core radius A
CoreRho=ParticlePar2                   // rho for core material
Shell1Rho=ParticlePar3                 // rho for shell 1 material
Shell2Rho=particlePar4                 // rho for shell 2 material
SolventRho=ParticlePar5                // rho for solvent material

```

"Janus CoreShell Micelle 3" ... particle size is radius of the core (R_i in the figure in description), parameters:

```

Shell_Thickness=ParticlePar1           //shell thickness A
CoreRho=ParticlePar2                   // rho for core material
Shell1Rho=ParticlePar3                 // rho for shell 1 material
Shell2Rho=particlePar4                 // rho for shell 2 material
SolventRho=ParticlePar5                // rho for solvent material

```

The reason for the two implementations is, that in usual implementation the shell thickness is fixed while the particle size has size distribution - but this is possible ONLY if core has distribution of sizes. This may be incorrect, as someone can have monodispersed cores, but distribution of shell thicknesses.

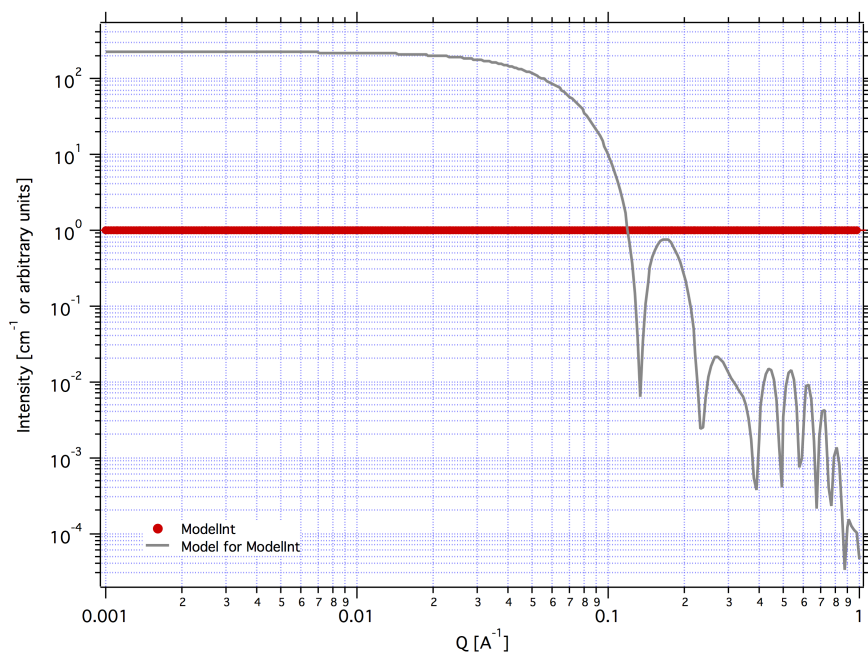
Note, that the "Janus CoreShell Micelle 2 and 3" will not work with some of the tools in Irena as all assume size represents total size (core+shell). Be warned, results will be difficult to present meaningfully! You are on your own...

Model comparison:

Core (Au): $131.5 \cdot 10^{10} \text{cm}^{-1}$
 Shell 1 (Al₂O₃) $34.95 \cdot 10^{10}$
 Shell 2 (ZrO₂) $46.27 \cdot 10^{10}$
 Solvant (H₂O) $9.42 \cdot 10^{10}$
 volume = 0.05

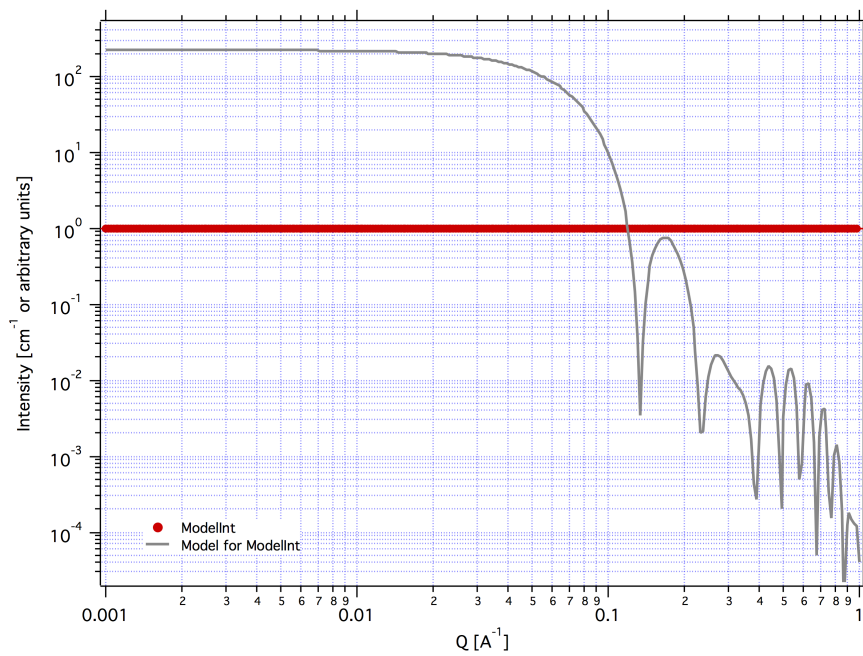
Janus CoreShell Micelle 1:

Mean radius 40Å, width 0.3Å (Gauss), Shell thickness 10Å,

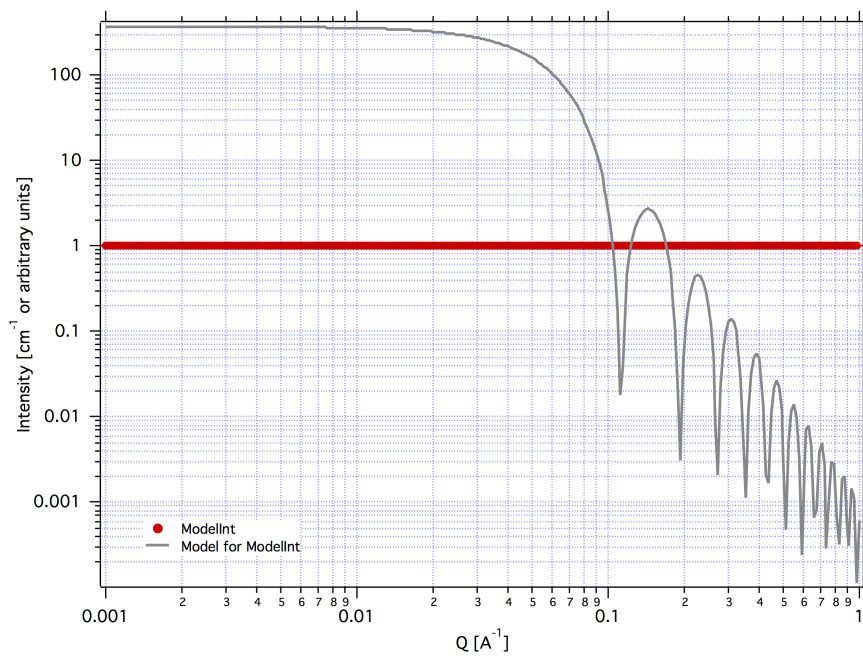


Janus CoreShell Micelle 2:

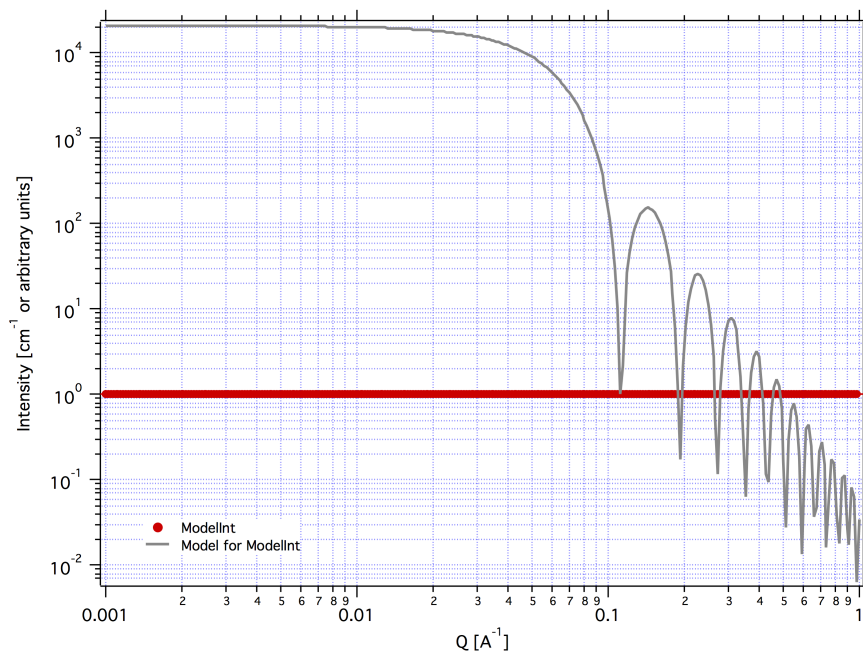
Core radius 30Å, Mean radius 40Å, width 0.3Å (Gauss) :



Janus CoreShell Micelle 1:
Pseudo sphere (shell thickness = 0), Radius = 40 A,

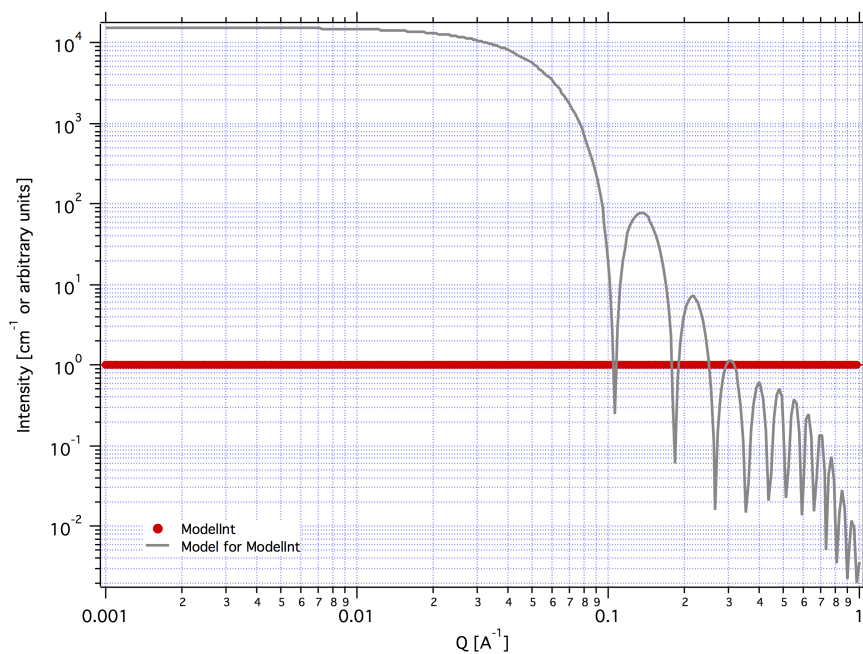


Real sphere, contrast 14903.5 (Au-water):

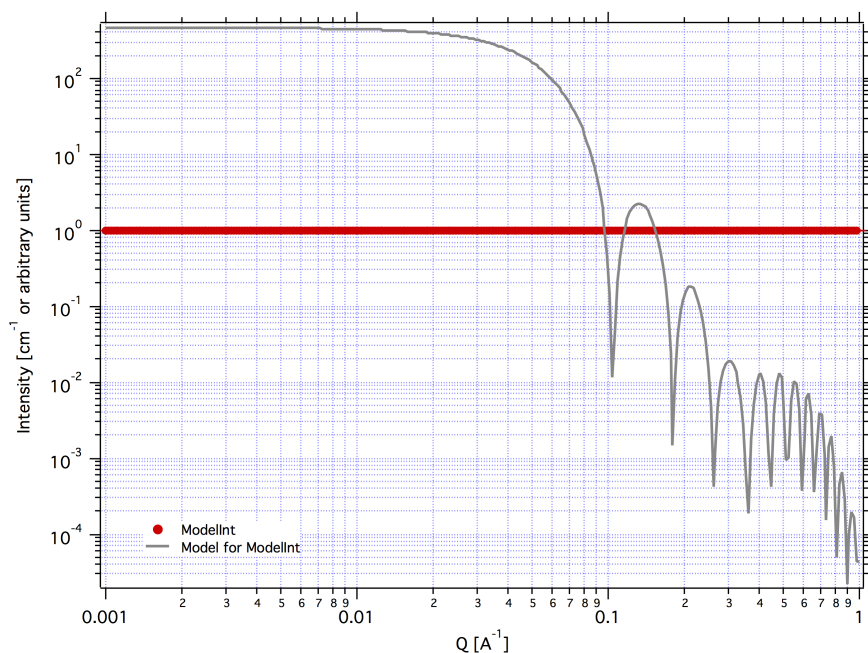


Note the suspicious difference in calibrations. See note above about my suspicion on the problem here...

Real core shell system (pick shell contrast 34.95). Use "Whole particle" as volume.



Janus CoreShell Micelle 1, fake the core shell with same contrast (34.95) for both shells. Recall that the total size of the CoreShell in Irena is radius of core ("Radius")+ shell thickness; while for Janus CoreShell Micelle 1 it is just Radius (see figure).



The difference in absolute intensity here is surely related to different assumptions on volume of particle.

```
*****
*****
*****
*****
```

RectParallelepiped

This is form factor or rectangular Parallelepiped, cuboid shape with side $A \times B \times C$ and all angle 90 degrees.

This form factor is ONLY available if NIST form factor xop is installed on the computer. If you install NIST SANS package

http://www.ncnr.nist.gov/programs/sans/data/red_anal.html

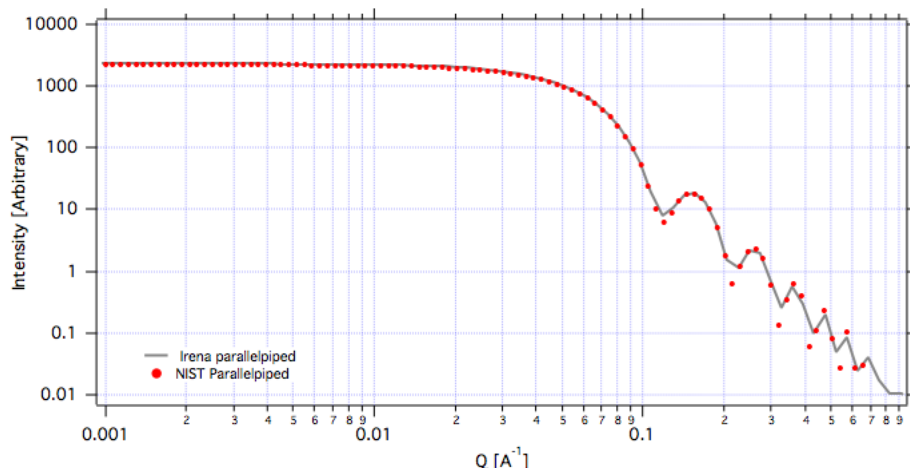
it installs xop which provides fast calculations of the various form factors. Since version 2.53 Irena will take advantage of some of these form factors.

In the case of rectangular Parallelepiped see NIST form factor description. It seems they had to go to original manuscript and recreate the form factor from the German original, Mittelbach and Porod, Acta Phys. Austriaca 14 (1961) 185-211, equations (1), (13), and (14) (in German!). Most publications citing this form factor seem to be wrong (I think there is error in Pedersen 1997 manuscript I was working with, Steven cites other manuscripts which seem to have bugs in them).

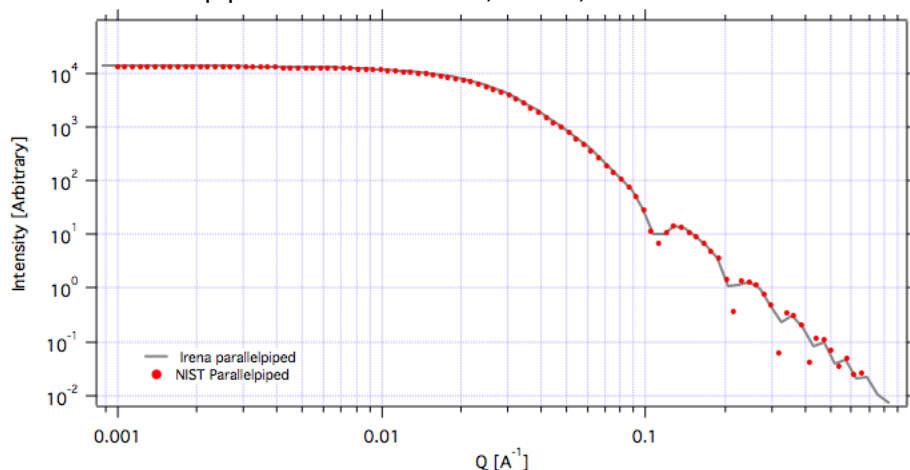
If you use this form factor, cite Steven Kline manuscript for NIST package: "Reduction and Analysis of SANS and USANS Data using Igor Pro", Kline, S. R. J Appl. Cryst. 39(6), 895 (2006).

Here is example of Form factor

Cuboid, 60A sides:



Hereis Parallelepiped with sides 60A, 120A, 180A:



Note, Irena assumed some size distribution (narrow, but some) while NIST package, assumes monodispersed particle. Therefore the differences in oscillations.

```
*****
*****
*****
*****
```

User

To use "User" form factor you will need to supply two functions:

1. Form factor itself
2. Volume of particle function

Both have to be supplied. Use of form factors which would include volume scaling within is possible, but MUCH more challenging due to other parts of code. If you really insist on doing so, contact me and I will create rules and explanation.

Both functions must work with radius in Angstroems and Q in inverse Angstroems.

Both have to declare following parameters, in following order:

Form factor: Q, radius, par1,par2,par3,par4,par5

Volume : radius, par1,par2,par3,par4,par5

These function are not required to use these 5 user parameters, but they have to declare them.

Examples for sphere:

```
Function IR1T_ExampleSphereFFPoints(Q,radius, par1,par2,par3,par4,par5) //Sphere
    variable Q, radius, par1,par2,par3,par4,par5
    variable QR=Q*radius
    return (3/(QR*QR*QR))*(sin(QR)-(QR*cos(QR)))
end

Function IR1T_ExampleSphereVolume(radius, par1,par2,par3,par4,par5) //returns
    variable radius, par1,par2,par3,par4,par5

    return ((4/3)*pi*radius*radius*radius)
end
```

```
*****
*****
*****
*****
```

Testing and using Form factors in users own code

To verify that the form factor works for you and to use the form factor if your own functions use following process and functions:

1. Generate Q wave with Qs for which the data are to be calculated
2. Generate intensity wave (will be redimesnioned as necessary, so the only thing is, it should be double precision).
3. Generate distributipon of radii wave - if you want to use single R, create wave with single point
4. decide what you want to calculate:

F^2	powerFct=0
$V * F^2$	powerFct=1
$V^2 * F^2$	powerFct=2

5. Run following command:

```
IR1T_GenerateGMatrix(R_FF,Q_wave,R_dist,powerFct,"form factor name",param1,param2,param3,param4,param5,
    "", "")
```

This function will return R_intensity, which is generally matrix with dimensions numpoints(Q_vector) x numpoints(R_dist), if R_dist has 1 point only, returned is wave (vector) as expected and reasonable...

The param1 - param5 are form factor parameters, as desribed in chapter 1, the "" at the end are for user form factor functions (there go the strings with names of user form factor and volume function).

"form factor name" is name from list in chapter 1.

6. Create log-log plot of the data if R_dist has single point. If R_dist has more point, well, you have to pull out the right column of data you need to plot.

Note, that if the IR1T_GenerateGMatrix function returns wave of NaN values if unknown name of form factor is passed in.

Example of code:

```
make/N=100 Q_wave
Q_wave=0.001+p/100
//will create 100 points wave with values 0.001 to 1) values
Make/O/D R_FF
//makes some place for form factor
make R_dist
R_dist=50
//or
//make/N=3 R_dist
//R_dist={10,50,100}
//creates R distribution and sets values
IR1T_GenerateGMatrix(R_FF,Q_wave,R_dist,powerFct,"form factor name",param1,param2,param3,param4,param5,
"", "")
//Note, above lines belong on one line together!
// replace powerFct with 0, 1, or 2!
// replace "form factor name" with name of form factor you want to use
Display R_FF vs Q_wave
ModifyGraph log=1
//creates log-log graph of
```

```
*****
*****
```

Structure factors description

This is list of library of structure factors. These structure factors enable to deal with limited S(Q) effects in Irena package. The functionality is provided by library, which can be called by any other user code. The library provides also GUI for setting the user parameters. In principle, further structure factors can be added if they have less than 5 parameters.

```
*****
*****
```

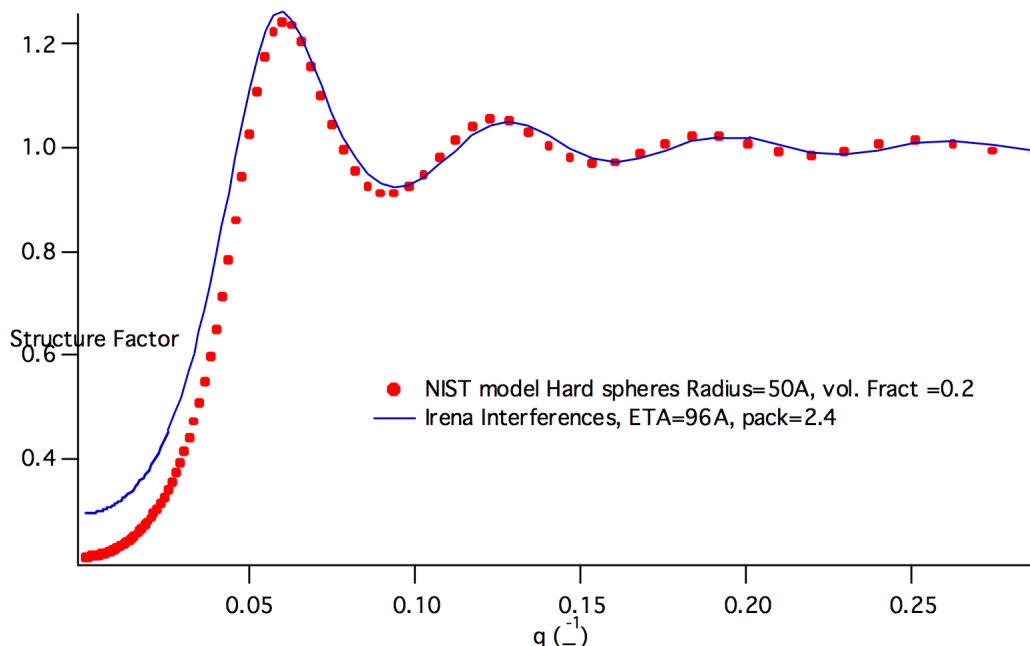
Interferences

This is original structure factor in Irena package. It has been provided as part of Unified fit model by Gregg Beaucage and is listed in his publication: Beaucage, G. (1995). Chapter 9 in ÅgHybrid Organic-Inorganic CompositesÅh, ACS symposium Series 585, edited by J. E. Mark, C. Y-C. Lee, and P. A. Bianconi, 207th National Meeting of the American Chemical Society, San Diego, CA, March 13-17, 1994. American Chemical Society, Washington, DC 1995. Pg. 97 – 111.

$$S(Q) = \frac{1}{1 + k * \frac{3 * (\sin(Q\xi) - Q\xi \cos(Q\xi))}{(Q\xi)^3}}$$

Note, that this model is, for most practical purposes, close to Hard spheres model with

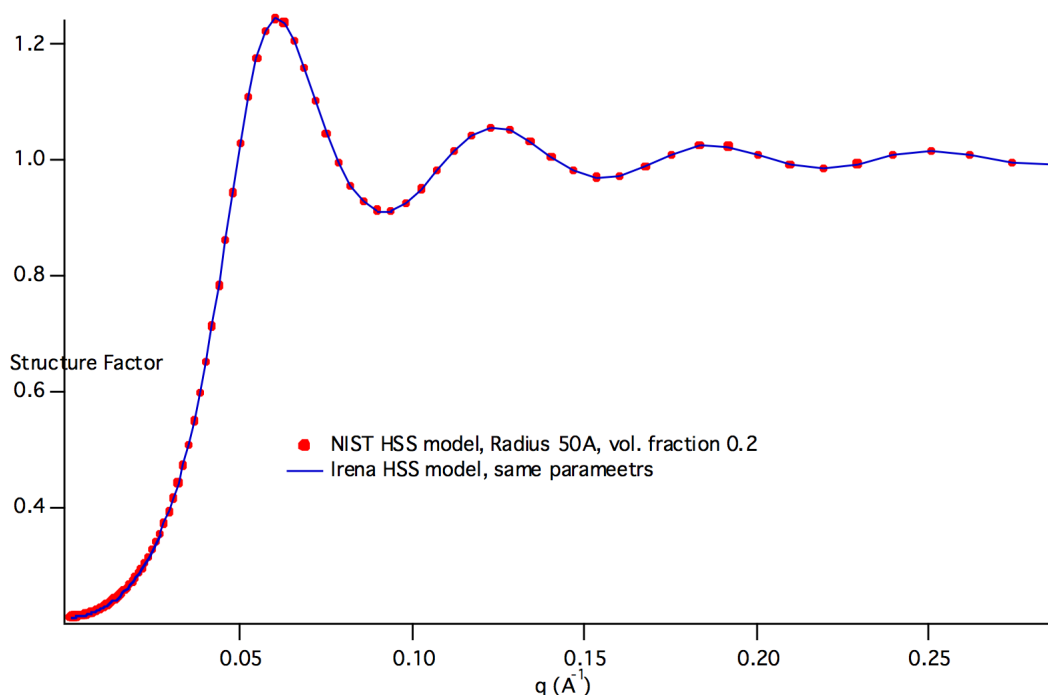
different definition of the parameters k ($\text{\AA}^3 \text{pack} \text{\AA}^3$) and f ($\text{\AA}^3 \text{ETA} \text{\AA}^3$). Modeling II extends the capabilities by including three more structure factors using code available from NIST Igor package (ref). Included are now: Hard spheres, Square Well, and Sticky Hard Spheres, which can be used in addition to interferences model above and no structure factor (dilute limit).



HardSpheres

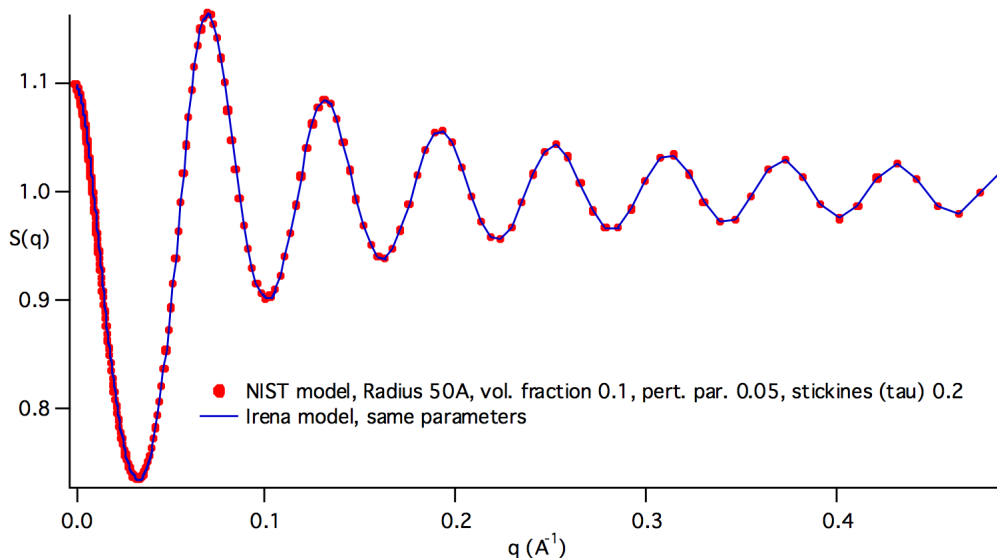
The code for this structure factor has been copied from NIST SAS macros (Kline, S. R. (2006). J Appl Crystallogr **39**, 895-900). Please, give them credit when using this structure factor. (http://www.ncnr.nist.gov/programs/sans/data/data_anal.html)

This is graph of NIST model and Irena implementation.



StickyHardSpheres

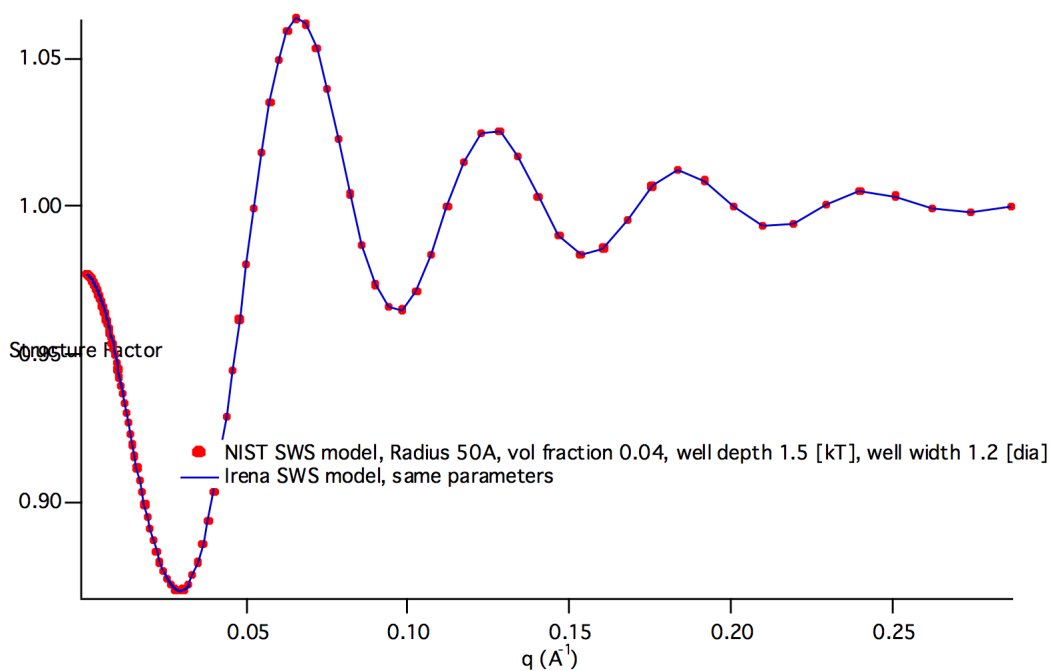
The code for this structure factor has been copied from NIST SAS macros (Kline, S. R. (2006). J Appl Crystallogr **39**, 895-900). Please, give them credit when using this structure factor. (http://www.ncnr.nist.gov/programs/sans/data/data_anal.html)



SquareWell

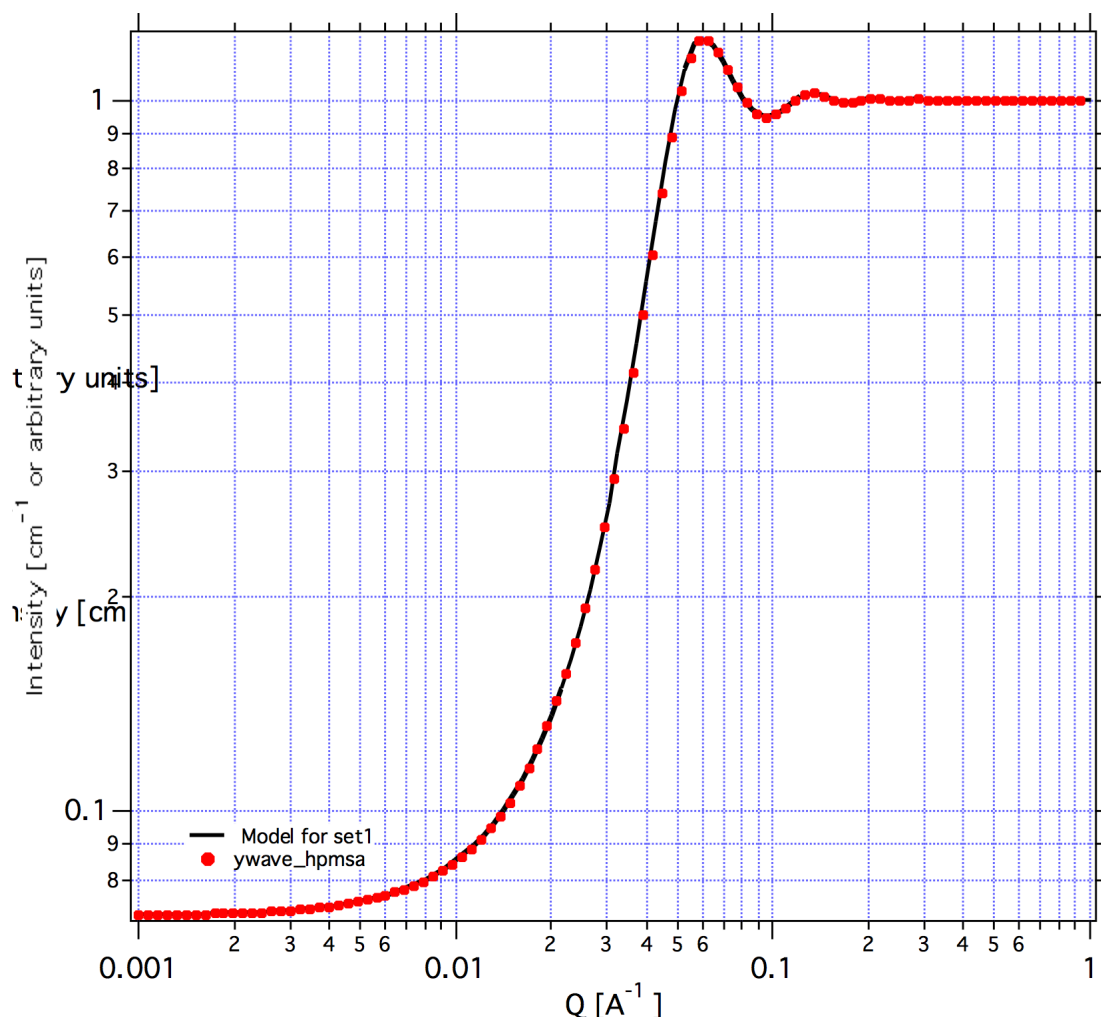
The code for this structure factor has been copied from NIST SAS macros (Kline, S. R. (2006). J Appl Crystallogr **39**, 895-900). Please, give them credit when using this

structure factor. (http://www.ncnr.nist.gov/programs/sans/data/data_anal.html)Åc



HayerPenfoldMSA

The code for this structure factor has been copied from NIST SAS macros (Kline, S. R. (2006). For any details on the use of these, please see the original code and description from NIST data analysis package (http://www.ncnr.nist.gov/programs/sans/data/data_anal.html)Åc Please, give them credit when using this structure factor.



This is graph from standard NIST set of parameters for both Irena package (black line) and NIST package (red dots).

Both assume ONLY structure factor (Form factor is set to 1). The parameters were:

Diameter (Å) 41.5 NOTE: Irena uses here radius, which is converted to diameter inside the structure factor.

This is to keep consistency with other structure factors.

Charge 19

Volume Fraction 0.0192

Temperature(K) 298

monovalent salt conc. (M) 0

dielectric constant of solvent 78

Units are mentioned in the help for each file on the Structure factor panel (you may have to enable help on Mac, it is shown always on PC in the bottom left corner of the Igor window).

Important note: this is comment from original NIST code.

```
// *** NOTE *** THIS CALCULATION REQUIRES THAT THE NUMBER
// OF
```

```
// Q-VALUES AT WHICH THE S(Q) IS CALCULATED BE
// A POWER OF 2
```

```
//!!!! this is at this time NOT enforced in Irena implementation...
```

```
// I am not sure if this is really problem or not.
```

```
// How do I find out? Users need to test this for me and if necessary, I
// need to try it out.
```

```
// in my testing there was NO problem with the results when the number
// of q points was arbitrary number of points...
```

InterPrecipitate

The code for this structure factor has been created on user request for study of precipitation in metals. It is based on formula 6 from APPLIED PHYSICS LETTERS 93, 161904 (2008), Study of nanoprecipitates in a nickel-based superalloy using small-angle neutron scattering and transmission electron microscopy by : E-Wen Huang, Peter K. Liaw, Lionel Porcar, Yun Liu, Yee-Lang Liu, Ji-Jung Kai, and Wei-Ren Chen. This manuscript refers for this formula to paper by R. Giordano, A. Grasso, and J. Teixeira, Phys. Rev. A 43, 6894 (1991). I did not look up original reference, so check it yourself to make sure the formula is OK

Structure factor has two parameters - L distance and sigma - root-mean-square deviation (ordering factor):

The interprecipitate structure factor¹³ $S(\vec{Q})$ is expressed as a function of Q , L , and σ

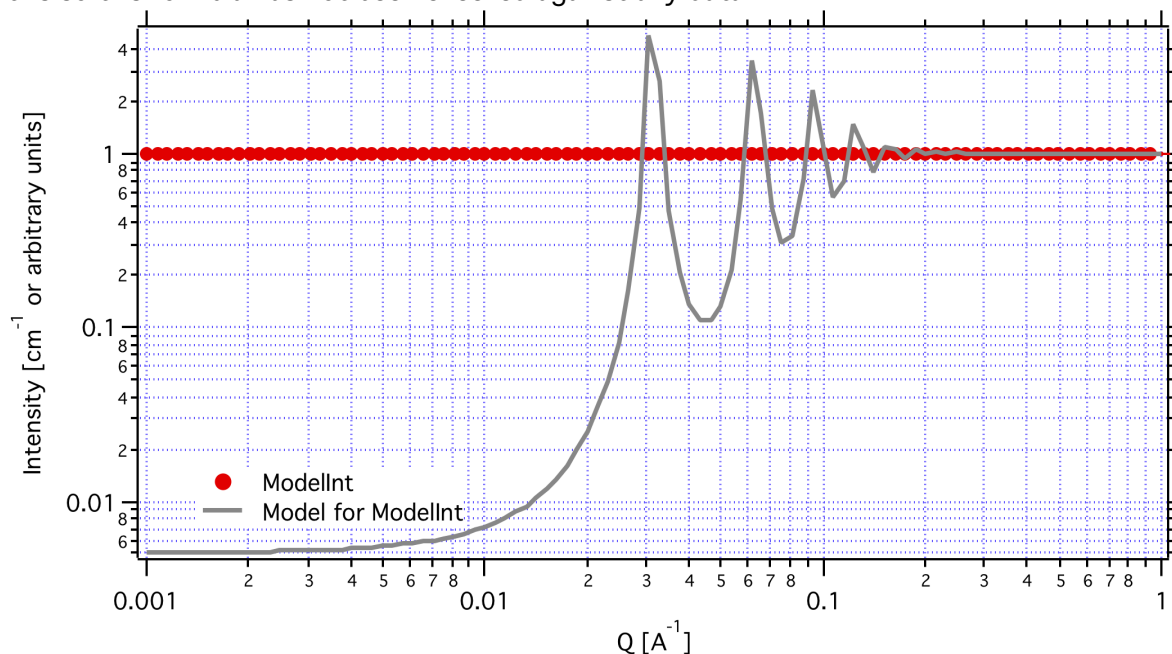
$$S(Q, L, \sigma) = 2 \left\{ \frac{1 - \exp[-(Q^2 \sigma^2)/4] \cos(QL)}{1 - 2 \exp[-(Q^2 \sigma^2)/4] \cos(QL) + \exp[-(Q^2 \sigma^2)/2]} \right\} - 1. \quad (6)$$

In Igor code this is programmed:

```
top = 1 - exp(-(Q^2*sigma^2)/4)*cos(Q*L)
bot = 1-2*exp(-(Q^2 * sigma^2)/4)* cos(Q*L) + exp(-(Q^2*sigma^2)/2)
```

$S(Q, L, \sigma) = 2*(top/bot) - 1$

This is model of the SF for L=200 and Sigma=20 (Sigma/L=10). I have no way of testing this so this formula has not been checked against any data.



Calling the library and use

Users can use built in library in their own code using following calls:

1. initialize by calling: IR2S_InitStructureFactors()

this is where the list of known structure factors is:

SVAR

ListOfStructureFactors=root:Packages:StructureFactorCalc:ListOfStructureFactors

2. use by calling:

IR2S_CalcStructureFactor(SFname,Qvalue,Param1,Param2,Param3,Param4,Param5,
Param6)

$I(Q) = I(Q, \text{dilute limit}) *$

IR2S_CalcStructureFactor(SFname,Qvalue,Param1,Param2,Param3,Param4,Param5,Param6)

//Dilute

system;Interferences;HardSpheres;SquareWell;StickyHardSpheres;HayterPenfoldMSA

3. Get panel by calling:

IR2S_MakeSFParamPanel(TitleStr,SFStr,P1Str,FitP1Str,LowP1Str,HighP1Str,P2Str
,FitP2Str,LowP2Str,HighP2Str,P3Str,FitP3Str,LowP3Str,HighP3Str,P4Str,FitP4Str
,LowP4Str,HighP4Str,P5Str,FitP5Str,LowP5Str,HighP5Str,
P6Str,FitP6Str,LowP6Str,HighP6Str,SFUserSFformula)

to disallow fitting of parameters, simply set FitP1Str="" etc.

then do not have to set low and high limits ...

Structure factors package...

IR2_OldInterferences this is roughly hard spheres (close to Percus-
Yevick model, not exactly), the $\text{ETA} = 2 * \text{radius}$ and $\text{Phi} = 8 * \text{vol. fraction}$ for PC
model.

IR2_HardSphereStruct this is Percus-Yevick model

IR2_StickyHS_Struct this is sticky hard spheres

IR2_SquareWellStruct this is Square well

IR2_HayterPenfoldMSA this is HayterPenfoldMSA

IR2_InterPrecipitateSF this is InterPrecipitate